

Design and Implementation of Three Phase Unbalanced Voltage Motor Controller

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Abstract— A state-of-the-art-technology was used to design the unbalanced three phase motor controller. The fluctuation of line voltage has been questioned in recent times due to the use of heavy powered machine with three phases. This paper is focused on deriving a control scheme to drive a three phase motor that could be used in industry or households. The very simple circuitry has been employed in this design. To do this, extensive MATLAB analysis and PSpice software was conducted in order to optimize the control system and finally the results are practically verified.

Index Terms— Industry, Line Voltage, Three Phase, Unbalance, Spark And Damage

I. Introduction

Fluctuations of line voltages are of special attention now-a-days. A need for reasonable power is required to smoothly operate electrical and electronic appliances. Quite often it happens that line voltages of some phases go down to a low level or high level. Therefore the line voltage becomes unbalanced. A large number of machines used in industries such as garments sectors, agricultural industry, cement factory, ceramic or glass factory, cold storage, dying sectors and so on are needed balanced voltage. For these erratic conditions of line voltages the valuable machines becomes damaged. Besides sometimes it makes sparking and makes serious problems in industry such as burning.

Under such erratic conditions of line voltage, in our country re-wireable fuse or miniature circuit breaker are normally used to protect different households from under and over-voltage conditions is explained in S. Islam et.al, [1]. Considering this factor, a protective device like over-voltage and over-current with time delay unit has been developed for ensuring a dependable and an effective protection to small households in year 1992 that explained in S. Islam et.al, [2]. This system is relatively slow and designed in transistor based. For the better performance another device has been developed to protect households in year 1994 which explained in S. Islam et.al, [3]. The operation speed of this device is better but it was designed in transistor based. In year 2011, another attractive device has been developed for single-phase line to protect electronic appliances from over-load which explained the author M.A.A. Mashud et.al, [4]. In this design transistor module has been replaced by IC module and use Hall Effect principle.

In year 2012, the author M.A.A. Mashud et. al, [5] explained single phase line voltage controller using microcontroller. In this design all electronic components and ICs has been replaced by using a microcontroller. But all the above designs are for single phase line voltage controller.

Now, the author developed a three phase unbalanced line voltage controller. Easily available components and simple circuitry, the system should be beneficial in providing low-cost.

II. Design Considerations

The system is divided into six main parts: low-voltage power supply, phase detector circuit, summing

circuit, reference voltage source, window detector circuit and relay driver unit. The block diagram and the complete circuit diagram of the developed system are depicted in Fig. 1 and Fig. 2 respectively.



Fig. 1: Block diagram of the developed system



Fig. 2: Complete circuit diagram of the developed system

2.1 Low Voltage Power Supply

Two types of low-voltage power supply are used in this design namely: positive and negative power supply. The positive low-voltage power supply circuit consists of transformer X_1 , D_1 , D_2 , D_3 , D_4 , C_1 , C_2 , and IC1 [6]. The output of the IC1 is +12V DC. The capacitor C_2 is connected across the output of IC1 to eliminate the high frequency noise. The negative low-voltage power supply circuit consists of transformer X_1 , D_5 , D_6 , D_7 , D_8 , C_3 , C_4 , and IC2. The output of the IC2 is -12V DC. The

capacitor C_4 is connected across the output of IC2 to eliminate the high frequency noise.

2.2 Phase Detector

Phase-I Detector

The phase-I detector circuit consists of transformer X_1 , D_9 , D_{10} , D_{11} , D_{12} , C_5 and VR1. The bridge rectifier circuit produces a pulsating DC voltage. Eliminating the pulsating DC produces pure DC by using capacitor

filter [7]. The filter capacitor C_5 is connected across the output of the rectifier circuit. A potentiometer VR1 is used for setting the output voltage to a desired value. In this design we have used this value to +2V DC denoted by V₁.

Phase-II Detector

The phase-II detector circuit consists of transformer X_2 , D_{13} , D_{14} , D_{15} , D_{16} , C_6 and VR2. The bridge rectifier circuit produces a pulsating DC voltage. Eliminating the pulsating DC produces pure DC by using capacitor filter. The filter capacitor C_6 is connected across the output of the rectifier circuit. A potentiometer VR2 is used for setting the output voltage to a desired value. In this design we have used this value to +2V DC denoted by V_2 .

Phase-III Detector

The phase-III detector circuit consists of transformer X_3 , D_{17} , D_{18} , D_{19} , D_{20} , C_7 and VR3. The bridge rectifier circuit produces a pulsating DC voltage. Eliminating the pulsating DC produces pure DC by using capacitor filter. The filter capacitor C_7 is connected across the output of the rectifier circuit. A potentiometer VR3 is used for setting the output voltage to a desired value. In this design we have used this value to +2V DC denoted by V_3 .

2.3 Summing Circuit

The summing circuit consists of R_1 , R_2 , R_3 , IC3 and VR4 [8]. In this design VR4 is used to minimize the output offset. The non-inverting configuration is employed in this work. The output voltage V_0 is equal to the sum of the input voltages applied to the non-inverting. The output voltage equation is expressed in equation (1) as follows:

$$\mathbf{V}_0 = \mathbf{V}_1 + \mathbf{V}_2 + \mathbf{V}_3 \tag{1}$$

2.4 Reference Voltage Source

Two types of voltage reference sources are used in this design i.e. lower limit level reference and upper limit level reference. The lower limit level reference source consists of Z_1 , R_4 , R_5 and VR5 [9]. The upper limit level reference source consists of Z_2 and VR6.

2.5 Window Detector

When it is needed to determine an unknown input between two precise reference thresholds V_{ut} and V_{lt} then window detector is used. The window detector circuit consists of IC4 and IC5 [10]. In this case the output summing circuit V_0 voltage is applied to the (-) input of IC5 and to the (+) input of IC4. An upper limit level reference voltage V_{ut} is applied to the (+) input of IC5, whereas the lower limit level reference voltage V_{lt} is applied to the (-) input of IC4. The outputs of IC4 and IC5 are connected to form a single output V_{0C} . When V_0 is between V_{ut} and V_{lt} the output V_{0C} is high. However, when V_0 goes above V_{ut} or drops below V_{lt} , the output V_{0C} switches low or to 0 V.

2.6 Inverter

The inverter is used to complement or invert a signal. It has a single input and a single output. The symbol and truth table for the inverter gate are shown in Fig. 3(a) and (b), respectively.



(b) Truth table

Fig. 3: (a) Symbol and (b) Truth table of an inverter

In the equivalent transistor circuit of Fig. 4 when a voltage is applied from the output of comparator to A, the transistor will be turned ON, drawing maximum collector current. Hence, whole of Vcc will drop across R thereby sending B to 0V. With 0V applied at A, the transistor will be cut OFF and the output B, therefore, will go to Vcc. Obviously, in each case, output is the opposite of input [11].



2.7 G. Relay Driver Unit

Transistor as a Switch

The transistor switch consists of Q_1 , Q_2 and R_6 . In an electronic circuit, the input signal (1 or 0) is usually

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applied to the base of the transistor, which causes the collector-emitter junction to become a short or an open circuit. When a transistor is used as a switch it must be either OFF or fully ON. In the fully ON state, the voltage V across the transistor is almost zero and the transistor is said to be saturated because it cannot pass any more collector current I_{CE} . The output device switched by the transistor is usually called the 'load'.

Calculation of Base Resistance, RB (R6):

The load resistance, which is the collector resistance, is the resistance of the relay coil as shown in Fig. 5.

The 12 V relay used has the coil resistance of 100 Ω . Therefore, $R = 240 \Omega$. The NPN transistor used is 2N3904. Thus, from the datasheet of 2N3904:

$$I_{c(max)} = 200 \text{ mA}, h_{FE(max)} = 300$$
 (2)

Taking h_{FE} to be 100 implies that

$$h_{FE} = 100, R_c = 240\Omega, V_{cc} = +12V$$
 (3)

But when the transistor is saturated

$$V_{CE(sat)} = 0.2V, V_{BE(sat)} = 0.7V$$
 (4)

Thus at saturation [12]

$$I_{c(sat)} = (V_{CC} - V_{CE}) / R_{C} = (12 - 0.2)/240 = 0.049$$
 (5)

Thus A = 49 mA

The minimum value of base current is then obtained

$$I_{B(min)} = I_{C(sat)} / h_{FE} = 49mA / 100 = 0.49mA$$
(6)

Therefore, the voltage across the base resistance R_B is

$$\mathbf{V}_{\mathrm{B}} = \mathbf{V}_{\mathrm{in}} - \mathbf{B}_{\mathrm{BE(sat)}} \tag{7}$$

When V_{in} is the output voltage of the inverter which is approximately equal to V_{cc} (+12V)

As a result, $V_B = 12 - 0.7 = 11.3V$, then the maximum value of R_B is

$$R_{B(max)} = V_B / I_B = 11.3 / 0.49 = 23.06 \text{ K}\Omega$$
 (8)

The maximum value of R_B that will allow a minimum I_B of 0.48 mA to flow was calculated by Ohm's Law. The actual value used should be much less. Therefore,

the base resistance, *R* was chosen to be 4.7 k Ω to ensure saturation which will give base current of

 $(12 - 0.7)V / 4.7 K\Omega = 2.48 mA > I_c /h_{FE}$ (i,e 0.49mA)



Fig. 5: Circuit diagram of the relay driver unit

Relay as a Switch

A relay provides total isolation between the triggering source applied to the terminal and the output. This total isolation is important in many digital or analog applications and it is a feature that certain semiconductor switches (e.g. transistors, diodes and integrated circuits) cannot provide. Also, the contacts are normally rated for currents much higher than the current rating of semiconductor switches [13].

Protective Diode

If the load is a motor, relay, or solenoid (or any other device with a coil), a diode must be connected across the load to protect the transistor from the brief high voltage produced when the load is switched OFF. In our design a protection diode D_{21} is connected 'backwards' across the load, in this case a relay coil. The diagram in Fig. 6 shows how a protection diode is connected 'backwards' across the load, in this case a relay coil [14].



Fig. 6: Illustration of a protection diode

The circuit of our design uses a relay to isolate an electric motor from the logic devices. Notice that the logic circuit and motor have separate power supplies. When the output of the inverter goes HIGH, the transistor is turned on and the NO contacts of the relay snap are closed. The motor operates by providing a rotary motion, which drives the mechanical devices that result in machine ON. When the output of the inverter goes LOW, the transistor stops conducting and the relay contacts spring back to their *NC* position. This turns off the motor, thereby stopping the machine.

III. Results and Discusion

The transfer function of three phase line voltage is implemented in Simulink (Matlab). The result is given in Fig. 7. This figure shows the line to neutral voltages and line to line voltage. Hence it seen that the line voltages is in normal condition.



Fig. 7: Simulation in Simulink

The complete hardware design is implemented and very satisfactory results are obtained. Firstly, the low voltage power supply unit was designed for highly regulated output to bias the major components of this system. In this design we had varied the input ac voltage from 198 volt to 248 volt but the output was remain constant at +12 volt and -12 volt DC. The experimented output waveforms of this unit are depicted in Fig. 8 and Fig. 9 respectively.



Fig. 8: Positive low-voltage power supply



Fig. 9: Negative low-voltage power supply

The reference voltage source was design in very confidently. In this design we had varied the input ac voltage from 198 volt to 248 volt and the output was observed and recorded. The lower-limit reference unit produces exactly 5.999 volt DC and the upper-limit reference unit produces exactly 6.001 volt DC. The practical output waveform of lower limit and upper limit reference voltage source is shown in Fig. 10 and Fig. 11 respectively.



Fig. 10: Lower-limit level refernce voltage



Fig. 11: Upper-limit level reference voltage

The output of the phase detectors circuit is shown in Fig. 12. From figure it is clear that phase-I, phase-II and phase-III produces exactly 2 volt DC when the line voltages are at normal condition that means no fluctuations in the line voltages. The output of the detector ciotcuit is measured by voltmeater and also osciloscope and obtained the result is very nearly to 2 volt DC.



Fig. 12: Output of phase detectors at normal line voltages (simulation)

The output of the detectors circuit is applied to the adder circuit. The adder circuit provides the output exactly equal to the sum of the input voltages. In this design, when no fluctuation occurs on the line voltages the adder circuit produce exactly 6 volt DC. In this case the output of the window detector is high (near to 11.5 volt). The transistor switched ON, hence the relay activated and the device is ON. The graphical representation of this condition is shown in Fig. 13. When the line voltages fluctuates, this may goes to up or down than the normal condition.



If the voltage of any one or more phase goes to down, the output of adder circuit becomes less than 6 volt (V_0 < 6 volt). The output of window detector is low (near to 0 volt). The transistor switched OFF, hence the relay turns OFF. Therefore the device becomes OFF. The graphical representation of this condition is shown in Fig. 14.



Fig. 14: Phase voltage goes down

If the voltage of any one or more phase goes to up, the output of adder circuit becomes greater than 6 volt ($V_0 > 6$ volt). Also the output of window detector is low (near to 0 volt). The transistor switched OFF, hence the relay turns OFF. Therefore the device becomes OFF. The graphical representation of this condition is shown in Fig. 15.



Fig. 15: Phase voltage goes up

IV. Conclusion

The system was successfully developed and was put under a series of tests for ascertaining its performance as a protective device. Its performance was strong and very satisfactory results were obtained. When any one of the three phases fluctuates, the motor was turned off. The safety of the equipment protection by the device under any undesired transient condition of the main supply was ensured. This device had a very high sensitivity. It was also simple in design, reliable in operation and cost competitive with any other product available in the market. From the above analysis, it is concluded that this device can easily protect three phase motor against fluctuation of line voltages and over load current.

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